

# Fault Analysis of Underground Cable System with Magnetic Shield Using Finite Element Analysis

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**Abstract:** In order to overcome the difficulties and problems especially the faults in overhead transmission systems which acts as intermediate link between generation and load end can be analyzed easily. Whereas in present day underground cables have attained greater importance because of reduced losses in distribution systems compared to overhead transmission lines. But the major problem in identifying the type of fault in these cables are quite complex. So for analyzing these faults in cables, a theory has been proposed based on installation of shields called magnetic shields in underground cables for fault detection and its classification in reference to overhead transmission lines. A detailed simulation by MTALAB/Simulink has been discussed. Finite elemental analysis is applied to the magnetic shield to determine the stress and strain in the shields which will be varying under abnormal conditions. The intensity of these stress levels determines the range of fault current which can be further verified by using Genetic and Chaotic algorithms.

**Keywords:** Transmission and distribution networks, Overhead transmission lines, underground cables, faults, shields, electromagnetic field theory.

## 1. Introduction

In this mechanized and modernized world electric power system has been enhanced a lot at different levels. The overhead transmission and distribution systems acts intermediate link between generation and loads, which contributes for 26% to 30 % of total losses and may affect the power systems performance adversely. Overhead systems are efficient for high voltages ranging from 66 KV to 765 KV. Whereas for the distribution network the overhead transmission system lacks sufficient right of way and becomes complex and further at the load end the conversion of radial to mesh takes place and increases the losses significantly. So in order to overcome this situation the utilization end can be modeled using underground cables where in the right of way doesn't play a major role, internal capacitance is greater than inductance results in suppression of electromagnetic interference.

Underground cables have achieved grater predominance because of their reduced losses. But the very problem is to analyze the behavior of the cables under fault conditions. Fault is defined as the disturbance which affects the performance of the systems abnormally. In this paper a concept called magnetic shield is considered and finite elemental analysis is performed to evaluate stress and strain.

## 2. Types of Magnetic Shields

Basically magnetic shields are classified based on type of source [1]

- Active Shield
- Passive Shield

And type of material used

- Ferromagnetic
- Paramagnetic
- Diamagnetic

Here ferromagnetic materials are considered of cylindrical in nature placed near junctions is considered the magnetic flux density due to conductor at point T in the direction of  $\psi$  given by [2]

$$B(T) = \frac{\mu_0 I}{4\pi\rho} (\cos \alpha_1 - \cos \alpha_2) \quad (1)$$

For simple shield geometry two dimensional modeling of the problem is sufficient, Cartesian coordinates can be used to model the long structures. Three dimension modeling must use at the edges of the structures (Cables, planner shields and bus bars). When active and passive shields are placed together in the transmission lines of conductive  $\sigma$ , the current density and electrical field are related by [2]

$$J = \sigma E \quad (2)$$

Quasi static magnetic fields are to be modeled by multi layering with high magnetic permeability, high electric conductivity or both.

The governing equations for vector of magnetic field and in a quasi-static [2] system are

$$\nabla \times \vec{H} = \vec{J} \quad (3)$$

$$\nabla \times \vec{E} = -j\omega\mu\vec{H} \quad (4)$$

$$\vec{E} = -j\omega\vec{A} \quad (5)$$

Where  $\vec{A}$  Is magnetic vector potential

$$\vec{B} = \mu\vec{H} = \nabla \times \vec{A} \quad (6)$$

The ratio between the resultant field after implementation [2] of shading and before implementation of shading

$$f_s = \frac{|\vec{B}_z|}{|\vec{B}_0|} \quad (7)$$

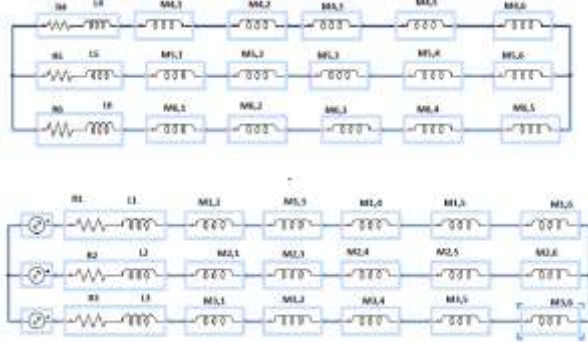
A smaller shielding factor  $f_s$  means better magnetic fields reduction. Shading factor above 1 means there is enhancement of magnetic fields and vice versa.

Considering a three phase underground cable with balanced

systems maintains balanced current under normal operating conditions and the current level increment to higher values under fault condition indicating the enhancement or reduction of magnetic fields.

### 3. Finite Elemental Methods

The name finite elemental analysis [3] itself is **self-explanatory** that the analysis is done on a finite element of the object. When considered a small finite element and performed stress analysis the behavior of that particular element will be reflected on the whole object. By implementation of this method mechanical analysis (force acting on particular point on the object) can be done easily. Mechanically while applying FEM the element behavior is observed between local axis and global axis. Whereas in electrical system the element behavior is analyzed between voltage and current, thus giving raises to the variation in potential energy. For the ease of detection in variation of physical properties, the shield material is modeled as the combination of resistance and inductance as shown below [2].



**Figure 1: Magnetic Shield**

Thus when the current passes through the shield material, it can apply resistant force against the force due to magnetic interference which is evident that shield material will experience stress or strain at fault location due to variation of fault current. Before the FEM is applied it is assumed that the object is sectioned in both x and y direction. The nodal displacement of each point is considered to be same. Thus the possibility to use the virtual displacement will be more. The displacement function can be chosen in the following form [4].

$$U = C_0 + C_1x \tag{8}$$

Applying the boundary conditions we have

$$U_1 = C_0 \text{ and } U_2 = C_0 + C_1l \tag{9}$$

Thus

$$C_0 = U_1 \text{ and } C_1 = \frac{U_2 - U_1}{l} \tag{10}$$

Then the displacement function for the single finite element can be written as

$$U = U_1 + \frac{U_2 - U_1}{l}x \tag{11}$$

$$U = U_1 \left(1 - \frac{x}{l}\right) + U_2 \frac{x}{l} \tag{12}$$

$$U = U_1N_1(x) + U_2N_2(x) \tag{13}$$

$N_1(x) = 1 - \frac{x}{l}$  and  $N_2(x) = \frac{x}{l}$  are known as nodal

functions. Thus the potential energy experienced by the element is given by

$$PE = \frac{1}{2} \begin{bmatrix} U_1 & U_2 \end{bmatrix} \begin{bmatrix} K_{11} & K_{12} \\ K_{21} & K_{22} \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \end{bmatrix} - \begin{bmatrix} F_m \\ F_e \end{bmatrix} \tag{14}$$

Where F matrix represents the magnetic force and electric force experienced by the element.

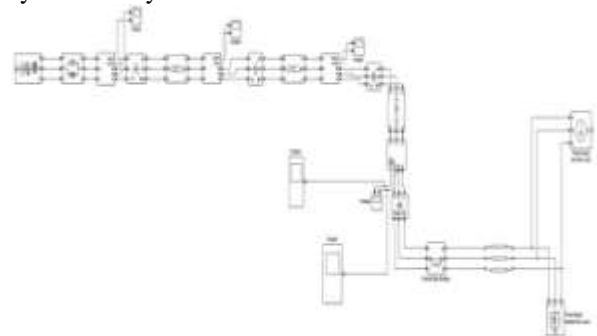
### 4. Optimization Algorithms

Generally optimization algorithms [5] are mainly applied to linear problems where the actual variables are originally formulated. Considering for instance a genetic algorithms where the characters that are determined at the genetic level by the way the parent chromosomes combine. In general populations of strings are used and are often referred as chromosomes and often simple analogies of genetic crossover and mutation are performed for each string in the population evaluated and the objective function is optimized. These are easily applicable for normal electrical systems. The very problem with linear algorithms is that some garbage bits at the coding positions gets attached to the stings to the optimal values and gets selected more often called hitch hiking bits. To overcome this effect chaotic optimization algorithm [6] is introduced which is nonlinear phenomenon and widely known for its dynamic properties namely ergodicity, intrinsic stochastic properties sensitive dependence on initial conditions. These factors accelerate the optimum seeking operation and find the global optimal solution.

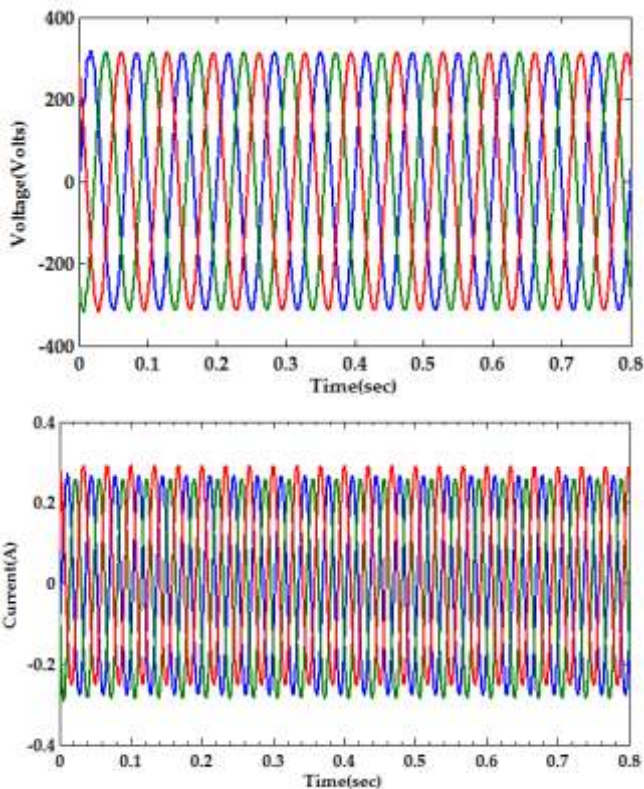
### 5. Results and Discussion

For the proper analysis and study regarding the faults on underground cables a proto type system has been considered consisting of both overhead transmission line and underground transmission line.

In the above diagram a 400 KV line transmission line has been considered and shown how it is distributed in different load type. Here the distribution end is considered that the transmission has been done with the underground cabling system. Matlab/Simulink simulations are carried out for the analysis of the system.

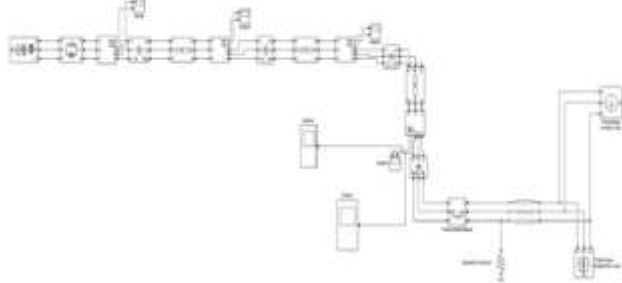


**Figure 2: System without Fault**

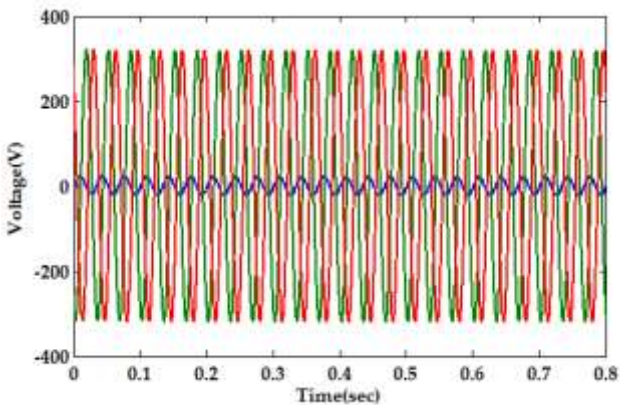


**Figure 3:** Voltage and Current Waveforms for normal System

Now when there is fault is introduced in the system there will be clear noticeable variation on voltage and current. Now when LG fault [6] is introduced in the system.

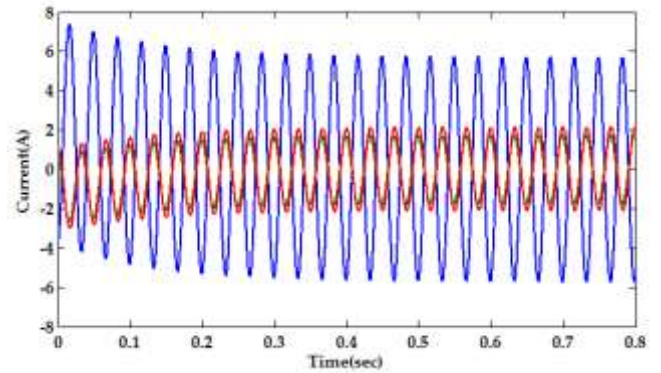


**Figure 4:** System with LG Fault

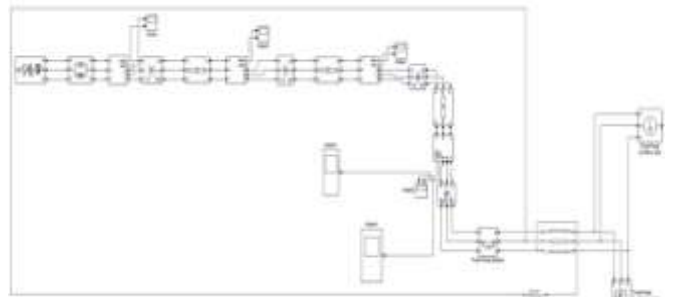


**Figure 5:** Voltage Waveforms during LG Fault

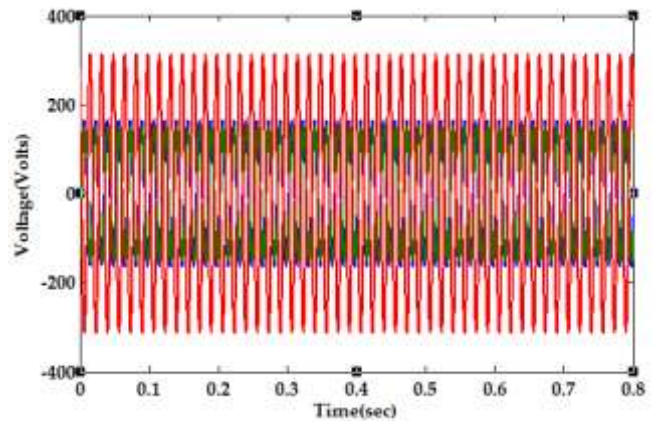
From the voltage waveforms it is clearly visible; the phase which is shorted with the ground has been dipped to almost to zero.



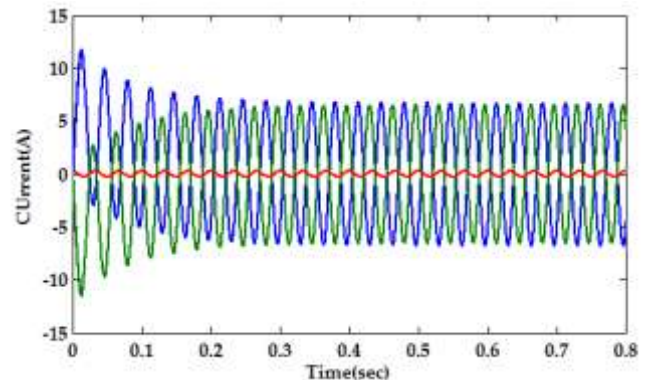
**Figure 6:** Current Waveforms during LG Fault  
 The phase which is grounded, there is hike in the current in system which is evident that it's a fault current. Now when LL fault is considered



**Figure 7:** System with LL Fault

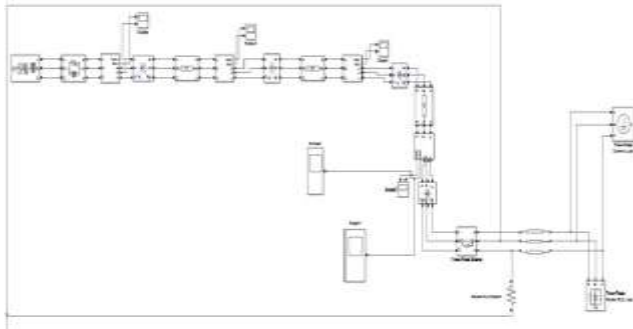


**Figure 8:** Fault voltage during LL Fault

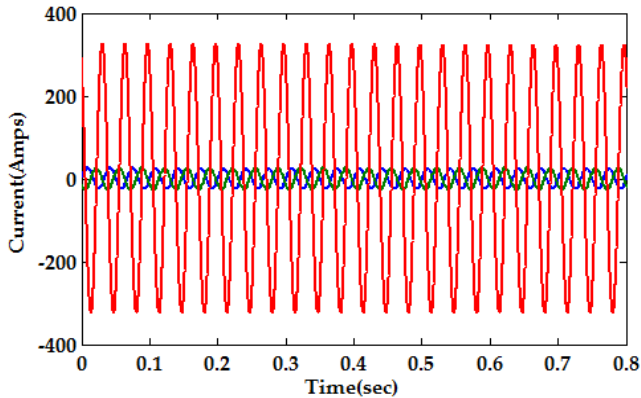


**Figure 9:** Current waveforms during LL Fault

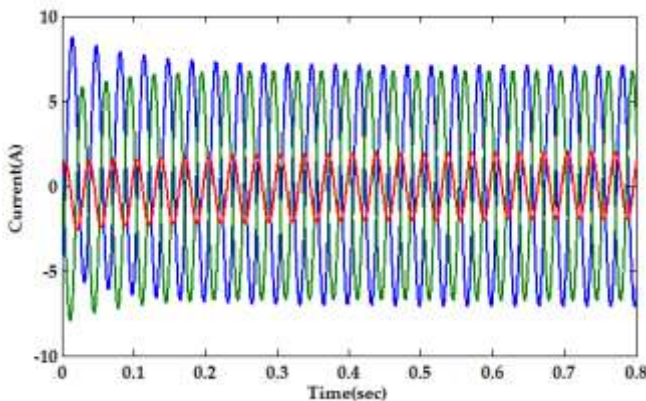




**Figure 10:** System with LLG fault

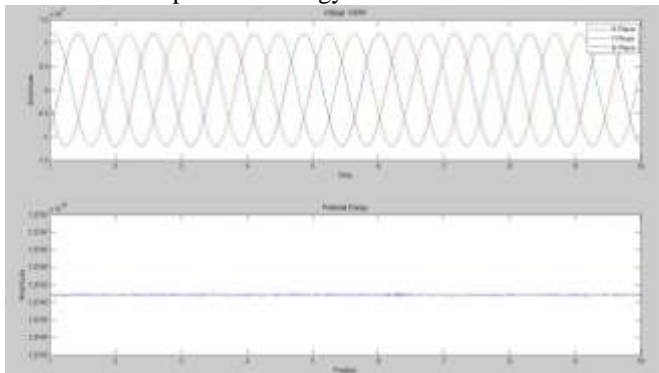


**Figure 11:** Voltage during LLG fault



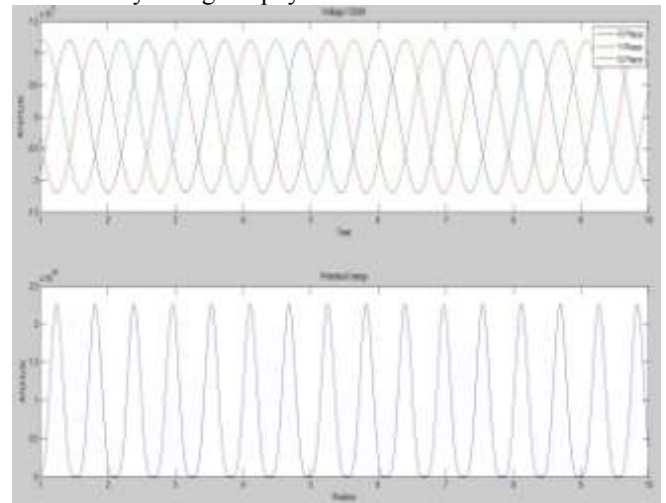
**Figure 12:** Current during LLG fault

The wave forms whatever were display in overhead system. Now taking these as reference underground cables will be designed. When finite elemental analysis is applied on a normal system the potential energy was constant throughout the cable. Now when any fault occurs then there will be variation in the potential energy.



**Figure 13:** Potential Energy Distribution during Normal Condition in the Shield

The above graph shows that the potential energy distribution along the shield is constant thought out. Thus during this condition shield will not apply any restraining force and there won't be any change in physical dimensions of the shield.



**Figure 14:** Potential Energy Distribution during fault Condition in the Shield

Now when there is fault is introduced in the cable system the potential energy distribution is not constant. This variation is enough for shield to change its physical properties.

**Table 1:** Comparison between Fem And Chaotic Optimizations With Respect To Shield Fault Currents

S.no	FEM SC in KA	Chaotic GA KA
1	380.16	418.52
2	352.718	351.58
3	321.3235	315.97
4	267.3519	289.08
5	153.1727	174.39

## 6. Conclusions

Magnetic shields are the most optimal protecting equipment with low cost that can be best utilized to find the underground faults of the system and it has been found that finite element method and chaotic optimization algorithms are yielding similar results. FEM applied on a small object can be applied on the entire shield.

## References

- [1] Frix W.M., Karady G.G., 1997, A Circuital Approach to Estimate @e Magnetic Field Reduction of Nonferrous Metal Shields, IEEE Transactions on Electromagnetic ComDatibility, Vol. 39. No. 1
- [2] Grover F.W., 1973, Inductance Calculations: Working Formulas and Tables, Research Triangle Park,NC: Instrumentation Society of America, Hasselgren L., Moller E., Hamnerius Y., 1994, Calculation of Magnetic Shielding of a Substation at Power Frequency Using FEM, IEEE Transactions on Power Delivery, Vol. 9, No. 3
- [3] Hoburg J.F.,et. al., 1997, Comparisons of Measured and Calculated Power Frequency Magnetic Shielding by

- Multilayered Cylinders, IEEE Transactions on Power Delivery, Vol. 12. No. 4
- [4] Moreno P., Olsen R.G., 1997, A Simple Theory for Optimizing Finite Width ELF Magnetic Field Shield for Minimum Dependence on Source Orientation, IEEE Transactions on Electromagnetic Comotabilim, vol, 39. No. 4
- [5] Mitigation techniques of power frequency magnetic fields originated from elec-tric power systems, Tech. Rep. Working group C4.204, International Council on Large Electric Systems (CIGRE), 2009
- [6] M.M. Dawoud, I.O. Habiballah, A.S. Farag, A. Fironz, Magnetic field management techniques in transmission underground cables, Electric Power Syst. Res. 48(1999) 177–192.
- [7] G.G. Karady, C. Nunez, R. Raghavan, The feasibility of magnetic field reduction by phase relationship optimization in cable systems, IEEE Trans. Power Deliv. 13 (2) (1998) 647–654
- [8] J.C. del Pino, P. Cruz, Influence of different types of magnetic shields on the thermal behaviour and ampacity of underground power cables, IEEE Trans. Power Deliv. 26 (4) (2011) 2659–2667.
- [9] E.C. Bascom, W. Banker, S.A. Boggs, Magnetic field management considerations for underground cable duct banks, in: Proc. IEEE Transmission & Distribution Conference, 2006, pp. 414–420.
- [10] J.C. del Pino, P. Cruz, Magnetic field shielding of underground cable duct banks, Prog. Electromagn. Res. 138 (2013) 1–19.[7]
- [11] M. Rachek, S.N. Larbi, Magnetic eddy-current and thermal coupled models for the finite-element behavior analysis of underground power cables, IEEE Trans. Magn. 44 (12) (2008) 4739–4746.
- [12] Canova, D. Bavastro, F. Freschi, L. Giaccone, M. Repetto, Magnetic shielding solutions for the junction zone of high voltage underground power lines, Electric Power Syst. Res. 89 (2012) 109–115
- [13] Impact of EMF on current ratings and cable systems, Tech. Rep. Working group B1.23, International Council on Large Electric Systems (CIGRE), 2013
- [14] G.J. Anders, Rating of Electric Power Cables. Ampacity Computations for Trans-mission, Distribution and Industrial Applications, McGraw Hill, New York, 1997.
- [15] C.C. Hwang, Numerical computation of eddy currents induced in structural steel due to a three-phase current, Electric Power Syst. Res. 43 (2) (1997) 143–148
- [16] G. Bertotti, Hysteresis in Magnetism, Academic Press, San Diego, CA, 1998.
- [17] N. Öztürk, E. C. elik, Application of genetic algorithms to core loss coefficient extraction, Prog. Electromagn. Res. M 19 (2011) 133–146
- [18] Y. Liang, Steady-state thermal analysis of power cable systems in ducts using streamline-upwind/Petrov-Galerkin finite element method, IEEE Trans. Dielectrics Electr. Insul. 19 (1) (2012) 283–290.
- [19] Electric cables – calculation of the current rating – part 3-2: Sections on operating conditions – economic optimization of power cable size, IEC Standard 60287.
- [20] P. Cruz, J. Riquelme, J.C. del Pino, A. de la Villa, J.L. Martínez, A comparative analysis of passive loop-based magnetic field mitigation of overhead lines, IEEE Trans. Power Deliv. 22 (3) (2007) 1773–1781
- [21] Juan Carlos del Pino López and Pedro Cruz Romero "A Comparative Analysis of Passive Loop-Based Magnetic Field Mitigation of Overhead Lines"
- [22] M Istenit, P Kokelj, P hnkob, B Cestnik, T iivic, "Some Aspects Of Magnetic Shielding Of A Transformer Substation Using Alternative Shielding Techniques"

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