Space Vector Pulse Width Amplitude Modulation for Boost Voltage Source Inverter

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Abstract: This paper proposes a space vector pulse width amplitude modulation (SVPWAM) method for a boost voltage source inverter. For a VSI, the switching loss is reduced when compared to a conventional sinusoidal pulse width modulation (SPWM) method. The output harmonic distortion of SVPWAM is lower than that of the SPWM, by using only one-third of the switching frequency compared to the latter one. As a result, it is feasible to use SVPWAM to make the boost inverter suitable for applications that needs high power density, high efficiency and low cost. The application includes DC power source utilization, power grid, induction heating and electric vehicle motor drive.

Keywords: Boost, SVPWAM, switching loss reduction, SPWM, harmonic distortion.

1. Introduction

In recent days the grid tie inverter technology has a vast development. Here the solar power which is a dc is converted to ac for tying with the grid. The inverter is required to inject low harmonic current to, in order to increase the efficiency. For this purpose, the switching frequency of the inverter is designed within a high range from 15 to 20 kHz, resulting in the increase in switching loss in the switching device.

To rectify this problem, different types of soft-switching methods have been proposed in [1]–[3]. A diode rectifier with small DC link capacitor have been proposed in [4], [5], [8]–[12]. Various types of modulation techniques have been proposed previously such as optimized pulse-width-modulation in [13], improved Space-Vector-PWM control for different optimization targets and applications [14]–[16], and discontinuous PWM (DPWM) [17]. Different switching sequence arrangement can also affect the harmonics, power loss and voltage/current ripples [18]. DPWM has been widely used to reduce the switching frequency, by selecting only one zero vector in one sector. It results in 50% switching frequency reduction. However, if the same output THD is required, DPWM cannot reduce switching loss compared to SPWM. It will also worsen the device heat transfer because the temperature variation. A double 120 flattop modulation method has been proposed in [6] and [7] to reduce the period of PWM switching to only 1/3 of the whole fundamental period. In addition to that, the method is only specified to a fixed topology, which cannot be applied widely.

This paper proposes a novel generalized space vector pulse width amplitude modulation (SVPWM) method for the boost voltage source inverter (VSI). By eliminating the conventional zero vector in the space vector modulation, two-third switching frequency reduction can be achieved in VSI. If a unity power factor is assumed, an 87% switching loss reduction can be implemented in VSI.

2. SVPWAM for VSI

A. Principle of SVPWAM Control in VSI

The principle of an SVPWAM control is to eliminate the zero vectors in each sector. The modulation principle of SVPWAM is shown in Fig.2. In each sector, only one phase leg is doing PWM switching; thus, the switching frequency is reduced by two-third. This imposes zero switching for one phase leg in the adjacent two sectors. For example, in sector VI and I, phase leg A has no switching at all.

The dc-link voltage thus is directly generated from the output line-to-line voltage. In sector I, no zero vector is selected. Therefore, S1 and S2 keep constant ON, and S3 and S6 are doing PWM switching. As a result, if the output voltage is kept at the normal three-phase sinusoidal voltage, the dc-link voltage should be equal to line-to-line voltage \( V_{ac} \) at this time. Consequently, the dc-link voltage should present a 60° varied feature to maintain a desired output voltage. A dc–dc conversion is needed in the front stage to...
generate this $60\degree$ voltage. The original equation for time period $T_1$ and $T_2$ are

\[ T_1 = \frac{\sqrt{3}}{2} m \sin \left( \frac{\pi}{3} - \theta \right) \]
\[ T_2 = \frac{\sqrt{3}}{2} m \sin(\theta) \]

The vector placement within one switching cycle in each sector is shown in Fig. 3 and 4 shows the output line-to-line voltage and switching signals of $S_1$.

### B. Inverter Switching Loss Reduction for VSI

For unity power factor case, the inverter switching loss is reduced by 86% because the voltage phase for PWM switching is within $[-60\degree, 60\degree]$, at which the current is in the zero-crossing region. In VSI, the device voltage stress is equal to dc-link voltage $V_{DC}$, and the current stress is equal to output current $I_a$. Thus the switching loss for each switch is

\[ P_{SW,1} = \frac{1}{2\pi} \int_{-\theta}^{\theta} E_{SR} \frac{V_{DC}}{V_{ref}} |i_a| |V_{DC}| f_{sw} \, d\omega + \int_{\pi/6}^{\pi/6} E_{SR} \frac{V_{DC}}{V_{ref}} |i_a| |V_{DC}| f_{sw} \, d\omega \]

\[ P_{SW,1} = \frac{2 - \sqrt{3}}{\pi} \left( \frac{l_m V_{DC}}{V_{ref} f_{ref}} \right) E_{SR} f_{sw} \]

where $E_{SR}, V_{ref}, I_{ref}$ are the references. Since the SVPWM only has PWM switching in two $60\degree$ sections, the integration over $2\pi$ can be narrowed down into integration within two $60\degree$

\[ P_{sw,1} = \frac{2\sqrt{3}}{\pi} \left( \frac{l_m V_{DC}}{V_{ref} f_{ref}} \right) E_{SR} f_{sw} \]

The switching loss for a conventional SPWM method is

\[ P_{sw,1} = \frac{2}{\pi} \left( \frac{l_m V_{DC}}{V_{ref} f_{ref}} \right) E_{SR} f_{sw} \]

In result, the switching loss of SVPWM over SPWM is $f = 13.4\%$. However, when the power factor decreases, the switching loss reduction amount decreases because the switching current increases. As indicated, the worst case happens when power factor is equal to zero, where the switching loss reduction still reaches 50%. In conclusion, SVPWM can bring the switching loss down by 50–87%.

### Topologies for SVPWM

Basically, the topologies that can utilize SVPWM have two stages: dc–dc conversion which converts a dc voltage or current into a 60\degree varied dc-link voltage or current; VSI for which SVPWM is applied. One typical example of this structure is the boost converter inverter discussed previously.

The front stage can also be integrated with inverter to form a single stage. Take current-fed quasi-Z-source inverter as an example. Instead of controlling the dc-link current $I_{dc}$ to have a constant average value, the open zero state duty cycle $D_{op}$ will be regulated instantaneously to control $I_{dc}$ to have a 60\degree fluctuate average value, resulting in a pulse type 60\degree waveform at the real dc-link current $I_{dc}$ since 11 is related to the input dc current $I_{in}$ by a transfer function.

### 3. Case Study: Boost Converter Inverter for Power Grid Application

#### A. Basic Control Principle

The circuit schematic and control system for a boost converter inverter for a power grid system is shown in Fig. 9. A 60\degree dc-link voltage is generated from a constant dc voltage by a boost converter, using open-loop control. Inverter could be modulated by a SVPWM method. The specifications for the system are input voltage is 39.2V; the average dc-link voltage is 78.6V; output line-to-line voltage rms is 89V.
B. Variable DC-Link SPWM Control at High Frequency

When the output needs to operate at a high frequency, between 120 Hz and 1 kHz, it is difficult to obtain a 6ω dc-link voltage without increasing the switching frequency of the boost converter. It is because the controller does not have enough bandwidth.

Also, increase in boost converter switching frequency would cause a substantial increase of the total switching loss, because it takes up more than 75% of the total switching loss. This is due to, the boost converter switches at a complete current region. Also a normal SPWM cannot be used in this range because the capacitor is designed to be small that it cannot hold a constant dc link voltage.

Therefore, its optimum option is to control the dc link voltage to be 6ω and do a variable dc link SPWM modulation. In this variable dc-link SPWM control, in order to obtain better utilization of the dc-link voltage, an integer times between the dc-link fundamental frequency and output frequency is preferred.

When the output frequency is in [60 Hz, 120 Hz], a 6ω dc link is chosen; when the frequency is in [120 Hz, 240 Hz], a 3ω dc link is chosen; when the frequency is in [240Hz, 360Hz], a 2ω dc link is chosen.

C. Experiment Results

![Prototype of SVPWAM-based boost-converter – inverter power grid connection](image)

**Figure 6: Prototype of SVPWAM-based boost-converter – inverter power grid connection**

**Output Waveform**

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Main Inductor</td>
<td>1</td>
<td>mH</td>
</tr>
<tr>
<td>Switches</td>
<td>MOSFET</td>
<td>IRF840</td>
</tr>
<tr>
<td>Microcontroller</td>
<td>ATMEL</td>
<td>AT89C51</td>
</tr>
<tr>
<td>Filter Capacitor</td>
<td>2200</td>
<td>µF</td>
</tr>
<tr>
<td>Load Resistance</td>
<td>1</td>
<td>kΩ</td>
</tr>
<tr>
<td>Input Voltage</td>
<td>39.2</td>
<td>V</td>
</tr>
<tr>
<td>Boosted Voltage</td>
<td>78.6</td>
<td>V</td>
</tr>
<tr>
<td>Output Voltage</td>
<td>89</td>
<td>V</td>
</tr>
</tbody>
</table>

D. Simulation Results

![Gate Pulses to Switches](image)

**Figure 8: Gate Pulses to Switches.**

![Line Voltage Waveform](image)

**Figure 9: Line Voltage Waveform**

![Phase Voltage Waveform](image)

**Figure 10: Phase Voltage Waveform.**

4. Conclusion

Hence the SVPWAM control method has the following advantages over the SPWM method.

1) The switching loss is reduced compared to the conventional SPWM inverter system.

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2) The overall cost is reduced by 30% because of reduced value of passive elements, usage of heat sinks.

The efficiency of the proposed method in the reduction of power losses has been tested by the experimental results that were obtained from the prototype model developed.

References


